Dependence of pH level on tribological effect of graphene oxide as an additive in water lubrication

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ABSTRACT

A study of the effectiveness of graphene oxides (GO) dispersed in water as a lubricant additive between tungsten carbide (WC) pin against stainless steel (SUS304) plate was carried out. A 0.1 wt.% GO was prepared and used as a lubricant under an applied load of 3 N for 20,000 friction cycles of reciprocating tribological testing. The results show that a GO dispersion with pH 3 provided the lowest friction coefficient, which was approximately 0.05. Worn areas on the wear track of the SUS304 flat plate and WC ball surface were also small. The increasing pH obviously affected the tribological properties, where the friction coefficient increased to approximately 0.10–0.20 in the steady state for pH 5, pH 7 and pH 9. Meanwhile, a GO dispersion with pH 10 was not able to provide good tribological properties for the tested materials. The observations on microscopic images revealed the formation of tribofilms on the wear tracks for low pH. The tribofilms caused reduction of the friction force and protected the plates from severe wear during the sliding tests.

Keywords: Graphene oxides; water lubrication; friction coefficient; pH; wear.

INTRODUCTION

The dependents of mechanical systems such as mechanical devices and metal-working on friction and wear reduction are highly considered. In order to accommodate strong demand in this area, studies of lubricants for lubrication systems have been widely carried out. Oil-based liquid lubricants have high lubrication abilities. However, oil-based lubricants present problems especially in terms of leaks and disposal, which have led to environmental problems [1]. Therefore, alternative lubricants need to be studied. Water is obviously the best candidate as an environmentally friendly liquid. The advantages of water for use as a liquid lubricant are its high cooling capacity, good fire-resistance, and low cost [2, 3]. However, there is a problem that the viscosity of water is too low to provide lubricating films between contact surfaces [4]. For this reason, several studies on additives to water to enable it to function as a lubricant have been carried out to address the problem [3, 5-8]. In recent years, carbon nanomaterials such as fullerene, carbon
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nanotubes (CNT), and graphene oxides (GO) have been studied as additives to water lubricants and have clearly shown good tribological properties [6, 9, 10]. These carbon nanomaterials have graphite structures composed of sp² bonding. Among the mentioned carbon materials, GO has received a lot of attention because of its unique properties, especially with lubricating potential [11, 12]. GO has many carbon oxygen functional groups, which allow for dissolution in water. The size of GO will also affect the dispersion level in water [13]. In addition, the pH level of GO dispersion in water will affect the dissolution in water. The pH level of GO dispersions synthesized by the exfoliating process becomes acidic [14]. High acidity is not desirable for application in metal parts because of the corrosion of metal surfaces. In this study, the tribological properties of a 0.1 wt.% GO dispersion in water were investigated using steel plates (SUS304) and tungsten carbide (WC) balls, which are generally used in metal-working. The influence of the pH level of GO dispersion on the tribological properties was discussed. Reciprocating sliding tests were carried out, and worn surfaces on both contact surfaces were investigated.

EXPERIMENTAL PROCEDURE

A tribometer shown in Figure 1 with a reciprocating sliding configuration was used to obtain the friction coefficients in this study. Friction tests were performed with a sliding displacement of approximately 2 mm, a sliding frequency of 300 rpm, and duration of 20,000 cycles, under an applied normal load of 3 N. Prior to the test, both the SUS304 flat plates and WC balls were cleaned in ethanol and then water for 5 min each using an ultrasonicator. The cleaned samples were placed in an acrylic box positioned on the sliding track of the tribometer. A sufficient amount of lubricant to cover the sliding area was added (approximately 2 ml). The acrylic box was covered and no water condensation was observed inside the box’s wall during the experiment, indicating no significant evaporation of the dispersion.

![Figure 1. Reciprocating tribometer used in the study](image)

The test materials used in this study were lapped stainless steel (JIS-SUS304) plates and sintered tungsten carbide (WC) balls with a diameter of 2 mm. The surface roughness (arithmetic mean roughness, \( R_a \)) of the lapped plate surfaces was
approximately 33 nm, and that of the ball surfaces was approximately 2 nm. Lubricated surfaces of the plates and balls after the sliding test were investigated by optical microscopy. All of the plates and balls were carefully washed by ultrasonicating in ethanol before the observation. The widths of the plate wear tracks were determined by the average of 3 measurements each at two different points. The concentration of the GO dispersion was 0.1 wt.% in this study. The pH regulation of the GO dispersion was carried out by adding alkaline solution, potassium carbonate (K₂CO₃), to the original pH 3 of the GO dispersion. The addition of alkaline solution was delicately conducted to adjust to pH 5, pH 7, pH 9 and pH 10. The effect of increasing the pH level of the GO dispersion was investigated.

RESULTS AND DISCUSSION

Figure 2 shows the SEM images of the original condition of GO flakes at pH 3 and the condition of GO flakes at pH 10. The SEM images were taken after the GO dispersions were dropped on silicon wafers and dried. There was no difference in the average size of over 25 μm of the GO flakes in both pH 3 and pH 10. The increase of the pH level of the dispersion caused agglutination of the GO flakes. This resulted in accumulation of the GO flakes on the silicon wafer.

![SEM images of GO flakes for pH 3 and pH 10](image)

Figure 2. SEM images of GO flakes for pH 3 and pH 10

Figure 3 is a graph of the friction coefficients against a sliding cycle using GO dispersion at various pH levels. The friction coefficients of all the samples of the GO dispersions were started at approximately 0.30. These friction coefficients were reduced in steady state for all of the dispersions except for pH 10. The best friction coefficient was obtained at pH 3 at extremely low 0.05 at the steady state. This was followed by pH
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5 and pH 7, which showed similar values of the friction coefficient. The friction coefficients of both dispersions were approximately 0.10. Meanwhile, pH 9 shows a longer running-in period, with the friction coefficient around 0.30. This friction coefficient was eventually reduced to slightly over 0.10 at 10,000 cycles. On the other hand, the GO dispersion with pH 10 showed the highest friction coefficient, which was 0.40 to 0.50. This friction coefficient is similar to that of water lubrication without any additive [6]. Therefore, the friction coefficient results indicate that the tribological performance provided by the GO dispersions deteriorated with increment of the pH level.

![Figure 3. Friction coefficient of 0.1 wt.% GO dispersions for various pH levels](image)

Figure 3. Friction coefficient of 0.1 wt.% GO dispersions for various pH levels

Figure 4 shows optical micrograph images of the wear tracks for the friction tests in the GO dispersions of pH 3, pH 7 and pH 10. The observation of micrograph images indicates that tribofilms were formed in the wear tracks by the GO dispersions for pH 3 and pH 7. Two types of tribofilm formed on the wear tracks for pH 3 and pH 7. One is an obvious thick black tribofilm, and the other is only slightly dark tribofilm. For pH 3, the thick tribofilm which formed half way along the sliding direction was observed and would provide an extremely low friction coefficient, 0.05. On the other hand, for pH 7, the wear track was mainly covered by slightly dark tribofilm, and the friction coefficient was 0.10. This friction coefficient is as low as that offered by conventional oil-based lubricants [6]. Similar tribofilms were not observed for pH 10. There was just noticeable severe wear along the sliding direction of the wear track. Therefore, the tribofilms provided good tribological properties on the contact surfaces of the sliding materials. Moreover, the formation of tribofilm is dependent on the pH level of the GO dispersion. This is due to the low pH levels, which will enhance the ability of GO to disperse in distilled water, as shown in Figure 2. As a result, the low pH levels will provide better GO dispersions and reduce the friction coefficient. However, instead of being evenly dispersed, the SEM images in Figure 2 showed an accumulation of GO flakes for pH 10. The conglomereration of GO flakes inhibited the formation of tribofilms between the contact surfaces.
Figure 4. Micrograph images of the wear tracks on plates and wear scar on balls for pH 3, pH 7 and pH 10 of GO dispersions.

The observations on WC balls are also shown side by side with the wear tracks in Figure 4. The differences of the wear that occurred on each ball surface were very clear. The formations of tribofilms on the wear track of pH 3 and pH 7 GO dispersions obviously protected the balls from greater wear. On the other hand, severe wear on the ball by pH 10 GO dispersion is found, which defined the poor tribological properties
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offered by the dispersion. Moreover, GO flakes substances seem to be adhered around the worn area of the ball, as shown by the arrow in the image of the WC ball for pH 10. The adherence of GO substances on the ball surface was probably from the conglomerated GO flakes for pH 10. Similar formations of substances were not observable around the wear areas on the ball for pH 3 and pH 7. This is because there were only the evenly dispersed GO flakes for pH 3 and pH 7.

Figure 5 shows the summarized data for friction coefficient, wear track depth and width for the GO dispersions with all the pH levels conducted in this study. These data were collected from at least 3 iterations of the tribological test for all GO dispersions. They were averaged to generate the comparison result. From the results, the pH 3 dispersions had a very low friction coefficient at 0.05. This was followed by pH 5 with 0.10. However, the amount of wear was approximately the same for both dispersions. On the other hand, although the friction coefficient for pH 7 was 0.10 in the graph of Figure 3, the averaged friction coefficient was 0.20. This was due to the variation in the data obtained in other samples. The friction coefficients of pH 7 and pH 9 were lower than that of pH 10. The results of the friction coefficients were also correlated to the depths and widths of the wear tracks, where the increment of friction coefficients absolutely increased the wear.

Figure 5. Summarized data of friction coefficient, depth and width of wear track by the friction test in GO dispersions (depth and width in μm)

CONCLUSIONS

In this study, the tribological properties of GO dispersions in distilled water with various pH levels were investigated using SUS304 steel plates and WC balls. The GO dispersion for pH 3 provided the lowest friction coefficient with low depth and width of the worn areas on the SUS304 steel plate and WC ball. However, the friction coefficients, wear on the balls and plates were all increased by the increment of the pH level. The good tribological properties achieved were supported by the formation of tribofilms on the wear tracks. The formation of tribofilms was highly dependent on the pH level of the GO dispersions, as the amount of K$_2$CO$_3$ is significantly low. However, an experiment with
diverse types of alkaline solution can be carried out for a clearer result for the solution’s effect on the friction coefficient. In addition, further modification to the chemical chain of GO will be conducted to increase their lubricity function as an additive for water lubricant.

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